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The running kinematics of free-roaming giraffes, measured using a low cost unmanned aerial vehicle (UAV)

Christopher K Basu ^{Corresp., 1}, Francois Deacon ², John R Hutchinson ¹, Alan M Wilson ¹

¹ Structure & Motion Laboratory, Royal Veterinary College, Hatfield, United Kingdom

² Faculty of Natural and Agricultural Sciences, Department of Animal, Wildlife and Grassland Sciences, University of the Free State, Bloemfontein, South Africa

Corresponding Author: Christopher K Basu
Email address: cbasu@rvc.ac.uk

The study of animal locomotion can be logistically challenging, especially in the case of large or unhandleable animals in uncontrolled environments. Recent technological advances have permitted the use of Global Positioning System and inertial sensors in locomotion studies, but these methods require manual access to each study subject. Here we demonstrate the utility of a low cost unmanned aerial vehicle (UAV) in measuring two-dimensional running kinematics from free-roaming giraffes (*Giraffa camelopardalis giraffa*) in the Free State Province, South Africa. We collected 120 Hz video of running giraffes, and calibrated each video frame using metatarsal length as a constant object of scale. We tested a number of methods to measure metatarsal length. The method with the least variation used close range photography and a trigonometric equation to spatially calibrate the still image, and derive metatarsal length. In the absence of this option, a spatially calibrated surface model of the study terrain was used to estimate topographical dimensions in video footage of interest. Data for the terrain models were collected using the same equipment, during the same study period. We subsequently validated the accuracy of the UAV method by comparing similar speed measurements of a running human subject, with a gold standard method. We recommend that future users maximise the camera focal distance, and keep the subject in the central field of view.

The studied giraffes used a grounded rotary gallop with a speed range of 3.4 to 6.9 ms⁻¹ (never cantering, trotting or pacing), and lower duty factors when compared with other cursorial quadrupeds. As this pattern might result in adverse increases in peak vertical limb forces with speed, it was notable to find that contralateral limbs became more in-phase with speed. Considering the latter pattern and the modest maximal speed of giraffes, we speculate that tissue safety factors are maintained within tolerable bounds this way. Furthermore, the angular kinematics of the neck were frequently isolated from the pitching of the body during running; this may be a result of the large mass of the head and neck. Further field experiments and biomechanical models are needed to robustly test these speculations.

1 **The running kinematics of free-roaming giraffes, measured using a low cost**
2 **unmanned aerial vehicle (UAV)**

3 Christopher K. Basu¹, Francois Deacon², *John R. Hutchinson¹, *Alan M. Wilson¹

4

5 ¹ Structure & Motion Laboratory, Royal Veterinary College, Hatfield, Hertfordshire, UK

6 ² Faculty of Natural and Agricultural Sciences, Department of Animal, Wildlife and Grassland
7 Sciences, University of the Free State, Bloemfontein, Republic of South Africa

8

9 Corresponding Author:

10 Christopher Basu

11 Royal Veterinary College, Hatfield, Hertfordshire, AL9 7TA, UK

12 Email address: cbasu@rvc.ac.uk

13

14 * Co-senior authors

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16 **ABSTRACT**

17 The study of animal locomotion can be logistically challenging, especially in the case of large or
18 unhandleable animals in uncontrolled environments. Recent technological advances have
19 permitted the use of Global Positioning System and inertial sensors in locomotion studies, but
20 these methods require manual access to each study subject. Here we demonstrate the utility of a
21 low cost unmanned aerial vehicle (UAV) in measuring two-dimensional running kinematics
22 from free-roaming giraffes in the Free State Province, South Africa. We collected 120 Hz video
23 of running giraffes, and calibrated each video frame using metatarsal length as a constant object
24 of scale. We tested a number of methods to measure metatarsal length. The method with the least
25 variation used close range photography and a trigonometric equation to spatially calibrate the
26 still image, and derive metatarsal length. In the absence of this option, a spatially calibrated
27 surface model of the study terrain was used to estimate topographical dimensions in video
28 footage of interest. Data for the terrain models were collected using the same equipment, during
29 the same study period. We subsequently validated the accuracy of the UAV method by
30 comparing similar speed measurements of a running human subject, with a gold standard
31 method. We recommend that future users maximise the camera focal distance, and keep the
32 subject in the central field of view. The studied giraffes used a grounded rotary gallop with a
33 speed range of 3.4 to 6.9 ms⁻¹ (never cantering, trotting or pacing), and lower duty factors when

34 compared with other cursorial quadrupeds. As this pattern might result in adverse increases in
35 peak vertical limb forces with speed, it was notable to find that contralateral limbs became more
36 in-phase with speed. Considering the latter pattern and the modest maximal speed of giraffes, we
37 speculate that tissue safety factors are maintained within tolerable bounds this way. Furthermore,
38 the angular kinematics of the neck were frequently isolated from the pitching of the body during
39 running; this may be a result of the large mass of the head and neck. Further field experiments
40 and biomechanical models are needed to robustly test these speculations.

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43 INTRODUCTION

44 Measuring gait parameters outside of the laboratory

45 Biomechanical measurements of animal locomotion are commonly performed under laboratory
46 conditions. Under these circumstances, confounding variables may be measured and/or
47 controlled. When studying animals, particularly undomesticated animals usually living in natural
48 habitats, the laboratory itself can become a confounding variable. Natural behaviours are less
49 likely to be expressed, and it is difficult to replicate the interactions between the animal and its
50 natural environment (e.g. temperature, light, substrate properties). In many cases it is not
51 logistically possible or safe to study animals in a laboratory setting.

52 In recent years, the increasing availability of remote sensing has broadened the focus of
53 locomotor research to include more field-based data collection. Accelerometers and Global
54 Positioning System (GPS) devices have been used to derive three-dimensional temporospatial
55 parameters in a variety of human (Tao et al. 2012) and non-human locomotor studies (Daley et
56 al. 2016; Hubel et al. 2016). Whilst these methods are an excellent solution to study locomotor
57 behaviours over an extended period of time, one challenge is that physical access to each study
58 subject is required. This inevitably requires an instance of either manual or chemical restraint.

59 If two-dimensional (2D) temporospatial kinematics are required, a low cost alternative is to use
60 an unmanned aerial vehicle (UAV) to gather spatially calibrated video footage of the locomotor
61 behaviour in question. In this study, we demonstrate the utility of a single low-cost UAV in
62 measuring the 2D kinematic gait parameters of free-ranging running giraffes (*Giraffa*
63 *camelopardalis giraffa*). We use these data to question whether giraffes' running gait is
64 specialised when compared with other mammalian quadrupeds.

65 Gait dynamics in giraffes and other quadrupedal mammals

66 Quadrupeds typically use asymmetrical gaits at faster speeds. In asymmetrical gaits the fore- and
67 hindfeet each act as functional pairs, where each pair of feet can strike the ground
68 simultaneously, or may have a time lag between the footfall of the left and right side, in which
69 case there is a leading and a trailing foot. Galloping gaits may be further defined by the pattern
70 of the leading limbs. In a transverse gallop, the leading limbs of the fore and hind quarters are on
71 the same side of the body, *versus* a rotary gallop where the leading limbs are on the opposite

72 sides of the body. In either case, both a gathered and extended aerial phase can be present, where
73 all feet are airborne (Hildebrand, 1977, Biancardi and Minetti, 2012).

74 At walking speeds, giraffes use a lateral sequence walk, which is dynamically similar to the slow
75 gaits of other mammalian quadrupeds (Basu et al. Under review). The theory of dynamic
76 similarity predicts that geometrically similar animals move with similar dimensionless stride
77 parameters at equivalent dimensionless speeds. Dimensionless speed is expressed here as Froude
78 number (Eqn 1), where u = speed (ms^{-1}), h = shoulder height (m) and g = acceleration due to
79 gravity (9.81 ms^{-2}).

$$80 \quad Fr = \frac{u^2}{gh} \quad \text{Eqn 1}$$

81 Giraffes appear to diverge from the predictions of dynamic similarity at faster than walking
82 speeds. Instead of using an intermediate speed gait, such as a trot, giraffes seemingly transition
83 consistently from a walk to a rotary gallop (Dagg & Vos 1968; Maxwell 1924). The restricted
84 choice of gait is in contrast to most other cursorial quadrupeds (Heglund & Taylor 1988;
85 Hildebrand 1976), but not exclusive to giraffes; for example elephants use the lateral sequence
86 walk across their entire speed range (Hutchinson et al. 2006). At near-maximal running speeds,
87 giraffes are thought to use lower mean stride frequencies (and consequently higher stride
88 lengths) than is expected for an ungulate of their body mass; an ability that may be facilitated by
89 their elongate limbs (Alexander et al. 1977).

90 Giraffes' long neck may have functional consequences with respect to the locomotor system.
91 Evolutionary elongation of giraffes' cervical vertebrae has effectively lengthened their horizontal
92 axis (Badlangana 2009). In other galloping quadrupeds, the horizontal axis of the skeleton is
93 dynamic, where fluctuations in neck angle and body pitch occur during walking and running
94 (Dunbar 2004; Dunbar et al. 2008). Such angular fluctuations may serve to stabilise these axial
95 body segments in world space. In giraffes, Dagg noted the periodic angular fluctuations of the
96 neck, and found this to be larger in magnitude during the gallop than in the walk (Dagg 1962).
97 One way to define this effect of neck and pitching angles on the horizontal axis is to determine
98 the phase relationship between the kinematics of the trunk and the neck (Basu et al. Under
99 review).

100 Our aims in this study are to (1) validate the use of a UAV in measuring temporospatial gait
101 parameters and suggest recommendations for optimising data quality; (2) determine which

102 running gait(s) the giraffes select across their speed range, (3) determine how stride parameters
103 change within the running gait, (4) assess whether giraffes' running gait is specialised compared
104 to other cursorial quadrupeds, and finally (5) measure the angular kinematics of the neck and
105 body, and predict how their phase relationship contributes to body segment stability.

106
107

108 **MATERIALS & METHODS**

109 Video data of giraffes' running gait were recorded from three field sites in the Free State
110 Province, South Africa. A total of 35 giraffes were available for study; these varied in age, size
111 and sex (Table 1). The experimental protocol varied between the field sites, and was dependent
112 on the giraffes' degree of familiarity with people. A Phantom 4 UAV (DJI, Guangdong, China)
113 was used to film giraffes' locomotion from a lateral viewpoint, at 120 Hz, 1920 x 1080 pixel
114 resolution, with a 20 mm lens. This was the maximum possible frame rate and image resolution
115 of any low-cost UAV (<£1000) at the time the study was conducted.

116 The giraffes were motivated to run using different methods. In field site 1 (Table 1), giraffes
117 were accustomed to following a vehicle as part of their usual routine. During data collection, a
118 vehicle was driven along a straight track at steady speed. A 200 m segment of this track was
119 outlined with white paint marks spaced at 2 m intervals. This speed of the vehicle was
120 periodically varied to induce different steady state running speeds. In field sites 2 and 3, the
121 giraffes were less habituated to humans and vehicles; in these sites the sound and proximity of
122 the UAV was sufficient to induce galloping for short distances.

123 **Ethical statement**

124 This study had ethical approval from both the Royal Veterinary College (URN 2016 1538) and
125 the University of the Free State, South Africa (UFS-AED2016/0063). A regional permit to study
126 giraffes was obtained from the Department of Economic Development, Tourism and
127 Environmental Affairs (DEDTEA, Free State Province, South Africa) was obtained (permit
128 number 01/34481). Data were gathered during a two week period in October 2016; that month
129 was chosen as it was during the dry season, and typically lacks the extreme low and high
130 temperatures seen at other times of the year. Measures were taken to minimise stress and danger
131 to the giraffes, and management personnel were present at each site at all times. Firstly, data
132 were gathered during cooler times of day to minimise the risk of heat stress. Secondly, giraffes

133 were only filmed in open habitats with minimal ground obstructions. Thirdly, individual giraffes
 134 were only motivated to run up to twice daily, and for sustained periods of time less than one
 135 minute. In between bouts of data collection, giraffes were allowed to express normal behaviour.
 136

137 **Video calibration**

138 Prior calibration of UAV mounted cameras is not possible, as the subject-to-camera distance is
 139 not constant as it is with a static camera. Three calibration methods were used, either in
 140 combination or isolation (Table 1). With each method, the distance from the metatarsophalangeal
 141 joint to the most caudal point of the calcaneus (MTP-C; Figure 1) was used to calibrate each
 142 frame of digitised video. The MTP joint centre was measured as the centroid of a circle drawn
 143 around the joint. Video footage was manually digitised using the DLTDV6 (Hedrick 2008) script
 144 for Matlab (MathWorks Inc., Natick, MA, USA) software, using a system of virtual markers
 145 (Basu et al., Under review). The giraffes' natural coat patterns were used to maximise
 146 digitisation repeatability.

147 The MTP-C distance was measured using method A, B or C. Method A used close range digital
 148 photography and a trigonometry calculation (Eqns 2 to 4) to estimate the size of MTP-C.
 149 Photographs (Canon EOS 500D, 18-200 mm 5.6f lens, Tokyo, Japan) were opportunistically
 150 taken of each giraffe, focusing on the hindlimb. For each photograph, the distance from the
 151 camera sensor to the subject's area of interest was measured using a laser rangefinder (Disto D5,
 152 Leica, Wetzlar, Germany), and the lens focal length was later retrieved from the image metadata.

$$153 \text{ horizontal angle of view } (^{\circ}) = 2 * \operatorname{atan} \left(\frac{\text{sensor size}}{2 * \text{focal length}} \right) \quad \text{Eqn 2}$$

$$154 \text{ horizontal field of view } (m) = 2 * \text{distance} * \tan \left(\frac{\text{angle of view}}{2} \right) \quad \text{Eqn 3}$$

$$155 \text{ photo calibration constant} = \frac{\text{horizontal field of view } (m)}{\text{number of horizontal pixels}} \quad \text{Eqn 4}$$

156

157 The pixel MTP-C distance was then measured in each photograph using ImageJ (Rasband 2009),
 158 and converted to estimated metric distance using the calibration constant from Eqn 4. This
 159 trigonometry method assumes that the camera sensor is perpendicular to the subject. It was not
 160 possible to quantitatively measure the optical axis of the camera; therefore, parallax errors may
 161 have affected the resulting calculations. To offset this error, the mean estimate was used to

162 calibrate video footage. Due to the close-range nature of the photographs, this method was only
163 suitable in field site 1, which had a more controlled and predictable environment.

164 In Method B, 2 m ground markers were used to calibrate 10 still frames from video footage of
165 each giraffe, as they moved parallel with the markers. MTP-C distance was estimated from these
166 frames, and the mean value used to calibrate subsequent video data. This method was only
167 possible in field site 1, where the giraffes could be led along the 200 m track.

168 Method C was used where the giraffes' locations and locomotion trajectories could not be
169 anticipated (field sites 2 and 3). After recording video data, a textured 3D mesh of the terrain was
170 produced using aerial photographs taken from the UAV during an aerial survey at 40 m altitude.
171 The derived models were created using the software package Pix4D (Lausanne, Switzerland),
172 which takes GPS stamped photographs as an input, and outputs scaled and textured 3D meshes
173 of the corresponding terrain, using a photogrammetry method. These models were used to
174 identify and measure prominent ground features, which could be cross-referenced with features
175 in digitised video, and subsequently used to measure MTP-C distance. The criteria for suitable
176 ground features were that they had to be within the sagittal plane of the giraffe, and be
177 distinguishable on the 3D mesh and the video (Figure 1).

178 **Kinematic data processing**

179 Footage from statically mounted videos has a fixed coordinate system, originating from one
180 corner of the video. Footage from a moving camera has no fixed coordinate system, as the
181 boundaries of the video change with each frame. To compensate for this, an in-plane static
182 ground point was digitised for each analysed stride, and the digitised coordinates translated
183 relative to this fixed point. Rotational transformation of digitised points was not performed, as
184 camera rotation during flight was corrected by a three-axis stabilised gimbal, which corrects the
185 pitch, yaw and roll of the camera to the nearest 0.02° (<https://www.dji.com/phantom-4-pro/info>).

186 This experimental setup allowed for a single lateral camera view. A consequence was that far
187 side foot-on events frequently were obscured; however far side foot-off events reliably were
188 visible. These data allowed contralateral limb phase (the lag between a pair of fore or hindlimb
189 footfalls) to be measured, however ipsilateral limb phase (the lag between fore and hind
190 footfalls) could not be measured, as this requires the foot on and off timings for all four feet to be

191 measured (Hildebrand 1977). The complete set of foot events were visible in one stride, which
192 was used to quantify the footfall sequence for the galloping gait. We defined a stride by the
193 timing from the nearside hindlimb foot-ground contact event, to the timing of the subsequent
194 nearside hindlimb foot event.

195 A number of criteria were used to ensure that stride data were suitable for analysis. An
196 assumption of linear regression is that the data units are independent from each other. To ensure
197 that this assumption was met, only one stride from a sequence of consecutive strides was used in
198 the analyses. A sequence of consecutive strides was defined as being bounded by either a change
199 in gait, or an obvious change in steady state speed. Only steady-state strides were analysed;
200 strides which featured a 20% or greater change in speed over their course were excluded. Speed
201 was subsequently measured as the horizontal displacement of the giraffes' withers over the
202 course of one stride (m), divided by the time interval (s).

203 Strides were manually segmented with a user-based determination of foot timings. Ideally a
204 velocity threshold method provides a repeatable method of detecting foot contact events (Starke
205 & Clayton 2015), but could not be used in this instance due to excessive measurement noise. A
206 custom-written Matlab script then applied the pixel calibrations and transformations to the raw
207 data. The following parameters were calculated: running speed (ms^{-1}), stride length (m), stride
208 frequency (Hz), footfall timings, contralateral limb phase (the fraction of the stride between
209 footfalls of leading and non-leading limbs), stride duration (s), stance duration (s), duty factor
210 (the fraction of the stride that a given foot is in contact with the ground), neck angle and body
211 pitch angle ($^{\circ}$).

212 The phase relationship between neck angle and body pitch was calculated as the percent
213 congruity. This is a measure of how often the slopes of neck angle and body pitch time series
214 share the same sign; indicating whether the respective angular patterns of the neck and body are
215 in-phase (high congruity) or out-of-phase (low congruity) (Ahn et al. 2004). Using the angle
216 convention defined in Figure 2A, 100% congruity represents simultaneous neck ventroflexion
217 and 'motor-bike' body pitching, whilst 0% represents simultaneous neck dorsiflexion with
218 upward body pitching.

219 **Comparisons with dynamic similarity**

220 Power equations were determined to fit Froude number to relative stride length (stride length/ leg
221 length), fore duty factor and hind duty factor. Plotted data from Figures 3 and 4 of Alexander and
222 Jayes (1983) were digitised using a web based application
223 (<http://arohatgi.info/WebPlotDigitizer>), and power curves were fitted to the resulting data, to test
224 how well our giraffe data fit those data for other mammals. The 95% confidence intervals of the
225 exponents and coefficients from the current dataset were compared with the corresponding
226 intervals from Alexander and Jayes' models of dynamic similarity (Alexander & Jayes 1983).

227 **Statistical analysis of stride parameters**

228 Statistical procedures were carried out using the Matlab Statistical Toolbox. All stride
229 parameters were tested for normality using a Kolmogorov-Smirnov test. Differences in fore or
230 hindlimb parameters were identified using a two-tailed t-test, and analysed separately if
231 statistically significant differences were present. OLS linear regressions were performed using
232 speed as the independent variable, and stride and force parameters as the dependant variable. To
233 compensate for multiple statistical comparisons, critical p-values were adjusted using the
234 Benjamini-Hochberg procedure, using a false discovery rate of 0.05 (Benjamini & Hochberg
235 1995).

236 **Method comparison and validation**

237 The precision of speed measurements was dependent on the precision of the MTP-C
238 measurements, i.e. the calibration method. The three calibration methods were compared in field
239 site 1, using one giraffe. In the case of method C, MTP-C distance was estimated separately
240 using both the artificial ground markers ($C_{ARTIFICIAL}$), and naturally occurring features
241 ($C_{NATURAL}$).

242 Method A (using close range photography) subsequently had the lowest standard deviation
243 between ten repeated measurements, and was used to quantify the percentage error of the other
244 methods:

$$245 \text{ Percentage error of Method}_{OTHER} = \frac{\text{Estimate}_{OTHER} - \text{Estimate}_A}{\text{Estimate}_A} * 100 \quad \text{Eqn 5}$$

246 We assessed the accuracy of UAV derived measurements of speed in a separate validation study,
247 based on Method A. The field conditions were approximated by measuring the speed of a human
248 subject as they ran on a treadmill. Written consent from the human participant was obtained.

249 Prior to the experiment, the subject's knee to ankle distance was measured using close range
250 photography and Eqns 2 to 4. Skin markers overlying the lateral femoral condyle and lateral
251 malleolus were used to aid digitisation, and the treadmill belt was marked in 0.5 m increments.
252 The speed of the treadmill belt was used as the 'gold standard' to which UAV derived speeds
253 were compared. Treadmill speed was measured using marker displacement (m) divided by time
254 (s). Subject speed was separately measured as in Method A, using a point on the subject's chest
255 and the treadmill belt markers to measure displacement. Each frame of video data was calibrated
256 using the subject's knee to ankle distance.

257 We performed trials under three conditions, where the focal distance and camera axis were
258 independently varied. In each condition, the subject was instructed to run through their
259 comfortable speed range on a treadmill. The treadmill speed was adjusted accordingly in stages.
260 In the first condition the Phantom 4 UAV was manually held (i.e. without a fixed support) at a
261 distance of 4 m from the subject, and for the second condition at 8 m distance. In both these
262 conditions the camera's axis was centred on the subject. In the third condition, the focal distance
263 was kept at 4 m, but the camera's focal axis was offset laterally so that the subject was recorded
264 in the lateral third of the camera's field of view. This final condition explicitly tested the effect of
265 parallax distortion on data accuracy.

266 Percentage error ($Speed_{ERROR}$) was defined from the gold standard measurements of speed
267 ($Speed_{GOLD}$) and measurements derived from the UAV ($Speed_{UAV}$):

$$268 \quad Speed_{ERROR} = \frac{Speed_{GOLD} - Speed_{UAV}}{Speed_{GOLD}} \times 100 \quad \text{Eqn 6}$$

269 We then tested the effects of camera focal distance and axis offset on percentage error, using a
270 two-way ANOVA.

271

272 **RESULTS**

273 Over 50 stride sequences were filmed, where the body and footfalls of at least one giraffe were
274 clearly visible. Data from 25 representative strides from four similarly-sized adult individuals
275 were included in the analysis (e.g. Video S1).

276 **Method comparison and validation**

277 Close range photography (Method A) yielded MTP-C estimates with the lowest standard
278 deviation (Table 2), and was used to estimate percentage error for Method B and C. The
279 percentage error of method B was 3.7%, with a 4 mm higher standard deviation than Method A.
280 When Method C (using a GPS calibrated terrain model) was applied using the artificial markers,
281 the percentage error was also 3.7%. The percentage error (5%) and standard deviation (0.1 m)
282 was larger when natural ground features (C_{NATURAL}) were used. Method A was subsequently
283 used to calibrate footage from field site 1, and method C_{NATURAL} was used for sites 2 and 3.

284 We compared speeds measured using a UAV with a gold standard method, using a human
285 running on a treadmill. Speeds measured with the UAV were consistently lower than treadmill
286 speed. Across all the experimental conditions, the mean measurement error was 13% of treadmill
287 speed. The condition with the highest mean error was condition 3 (focal distance of 4 m with an
288 offset axis) with an error of 17%; and the lowest was condition 2 (focal distance of 8 m), with an
289 error of 8%. Both camera focal distance and axis offset resulted in significant differences in
290 $\text{Speed}_{\text{ERROR}}$ (ANOVA $p < 0.0001$ and $p = 0.04$ respectively), with distance having the largest
291 effect (Figure 3).

292 **Giraffe running kinematics**

293 The observed speeds ranged from 3.4 to 6.9 ms^{-1} , with a mean of 5 ms^{-1} (or Fr 1.35). Given that
294 the individuals studied were of similar size, absolute speeds were analysed. Giraffes moving
295 immediately slower than this speed range used the lateral sequence walking gait, consistent with
296 previous observations in giraffes (Basu et al., under review). In the adult giraffes studied, the
297 observed running gait was a grounded rotary gallop (Figure 4). Brief aerial phases were only
298 observed in juveniles, and are not covered in the present analysis.

299 Linear regression results are reported in Table S1. A statistically significant increase in stride
300 length ($p < 0.001$) and stride frequency ($p < 0.001$) was observed (Figure 5), respectively
301 representing an increase of 0.5 m and 0.05 Hz for each 1 ms^{-1} increase in speed. Stance duration
302 (Figure 6A) was greater in the forelimb compared with the hindlimb ($p < 0.001$), and decreased
303 with speed ($p < 0.001$). In contrast, swing duration (Figure 6B) was shorter in the forelimb versus
304 the hindlimb ($p < 0.001$). There was however, no observed relationship between swing duration
305 and speed ($p = 0.8$). Duty factors (Figure 6C) and contralateral limb phase (Figure 7) decreased

306 with speed ($p < 0.001$ and $p = 0.002$ respectively), and were greater in the forelimb ($p < 0.001$ for
307 both parameters).

308 The body pitch fluctuation resembled a sine wave, and cycled once throughout the stride (Figure
309 2C), with an increase in pitching coinciding with the foot-off events of the forelimbs. The neck
310 angle oscillated once throughout the stride, although the pattern of change was more irregular
311 and more variable between strides (Figure 2B) than the body pitch angle. Neck range of motion
312 and body pitching did not vary as a function of speed ($p = 0.68$ and 0.07 respectively). Neck
313 angle and body pitch had a mean percent congruity of 70% (standard deviation 18%).

314 **Dynamic similarity**

315 Table 3 summarises the equations that describe how relative stride length and duty factors
316 changed with dimensionless speed in running giraffes. The coefficients and exponents were
317 compared with the predictive equations for dynamic similarity (Alexander & Jayes 1983).
318 Relative stride length in giraffes was consistent with these predictions. The coefficients (a)
319 describing ‘duty factor versus speed’ in giraffes were significantly lower than expected from the
320 models for dynamic similarity.

321

322

323 **DISCUSSION**

324 This study has highlighted the potential gains of using a UAV to collect field-based kinematics.
325 Using a moving *vs.* static camera allowed for a larger quantity of data to be recorded than would
326 otherwise have been possible. We have shown that speed and other 2D kinematic parameters can
327 be measured in this way. The major technical challenge was calibrating the raw footage to
328 calculate spatial parameters. The most consistent calibrations were gained when the study subject
329 was close enough to take repeated photographs, or when artificial markers were included in the
330 field of view. We tested the accuracy of this UAV method, and found that speed accuracy was
331 optimised at a longer focal distance, and when the subject was centred in the field of view
332 (Figure 3). Both of these conditions minimise the effect of parallax error on spatial
333 measurements (distances and angles). In addition to minimising error, long focal distances are
334 preferred to minimise potential stress to animal subjects. As a general rule, we recommend that

335 subjects are confined at least to the centre block of a 3x3 grid in the field of view (Figure 8),
336 whilst recognising the trade-off between focal distance and image resolution.

337 When close range photography or artificial ground markers are not feasible, a detailed 3D
338 textured mesh of the terrain may be used to calibrate the images, but this method resulted in an
339 additional calibration error of 5% (Table 2). An error of this magnitude does not alter our
340 findings about giraffe kinematics, but should be considered for future studies. The additional
341 error is related to the subjectivity of picking terrain landmarks which are visible in both the video
342 and 3D mesh. It is important that clearly visible ground features are used; this was illustrated by
343 the difference in error between using artificial ground markers *versus* naturally occurring
344 features (Table 2). A means to address this in future would be to increase the texture resolution
345 of the 3D mesh, to aid in identifying ground points. This can be done by conducting the aerial
346 survey closer to the ground, but as a trade-off, this demands more images per area, resulting in
347 longer flight times. As UAV battery life improves, this trade-off will become less important.

348 Camera sampling rate was also a limitation. 120 Hz was the standard for low-cost UAV
349 technology at the time of data collection. Whilst this was sufficient for measuring displacement
350 and speed across the stride, measuring the velocity or acceleration during foot contact events (for
351 the purpose of stride segmentation) resulted in excessive noise. In future, an interpolation
352 approach could be used to artificially increase the sampling rate.

353 Using this methodology, we were able to measure temporospatial parameters in free-roaming
354 giraffes without any physical contact. We found that giraffes' lack of an intermediate speed gait
355 (e.g. trot/pace) was compensated for by their rotary galloping gait, in that the walk-gallop
356 transition speed of approximately 3.4 ms^{-1} fell close to the mass-specific minimum trotting speed
357 observed in other mammalian quadrupeds (Heglund & Taylor 1988). For example, using Eqn 7,
358 a giraffe weighing 700 kg would be expected to have a minimum trotting speed of 3 ms^{-1} .

359 Minimum trotting speed = $0.593(\text{body mass}^{0.249})$ Eqn 7

360 In absolute terms, giraffes can be thought of as being slow gallopers (without routinely using a
361 cantering gait). Beyond the walk-to-gallop transition, increases in galloping speed were almost
362 exclusively achieved by increases in stride length; contrasting with the conserved range of stride
363 frequencies. This pattern is consistent in a wide range of quadrupedal running animals, and is
364 thought to reduce mass-specific energy costs (Heglund & Taylor 1988).

365 The giraffes in this study galloped with lower duty factors than predicted by dynamic similarity
366 (Table 3). It is tempting to suggest that giraffes experience similarly higher than expected
367 vertical peak ground reaction forces (GRFs) at equivalent speeds, because peak vertical GRF is
368 usually inversely associated with duty factor (Alexander 1984; Witte et al. 2004). Unfortunately
369 in giraffes it may not be possible to accurately predict peak GRF from duty factor alone. In our
370 previous work peak vertical GRF during walking was speed-independent; a finding which may
371 be related to limb compliance (Basu et al., under review). This could be explored in future with a
372 giraffe musculoskeletal model and a forward dynamics simulation in which peak GRFs are
373 simulated as a function of speed, as experimental data collection from giraffes galloping over
374 force plates may be logistically impossible. Such findings would have implications for muscle
375 power demands and tissue safety factors in giraffes.

376 Contralateral limb phase decreased with speed (Figure 7), resulting in a greater degree of overlap
377 between lead and non-lead footfalls. This is consistent with a peak GRF-minimising strategy,
378 where body weight is evenly distributed over two limbs during a greater proportion of the stride.
379 Such a mechanism would be particularly advantageous to giraffes, which possess a
380 disproportionately slender appendicular skeleton, and so may be sensitive to large skeletal
381 compressive and bending stresses (Biewener 1983; McMahon 1975).

382 The phase relationship between body pitch and neck angle was variable between trials, with a
383 mean congruity of 70%. Given that 100% congruity would represent in-phase neck ventroflexion
384 and positive body pitching, we speculate that the giraffe neck is inertially stabilised with respect
385 to a world frame, and is effectively decoupled from the motions of the trunk during running; a
386 similar situation to the energy-conserving mechanism observed during walking (Basu et al.). A
387 method of testing this idea in the future would be to examine the effect of ground incline, net
388 acceleration and high-speed turning on neck kinematics. Topography generated by the 3D terrain
389 mapping method used in this study would be particularly useful for this purpose. Alternatively,
390 the variation between strides with respect to phase, as well as the variation in neck angle (Figure
391 2B), may indicate an additional or different effect. Variation in angular neck kinematics during
392 galloping has also been noted by Dagg (Dagg 1962). Defining neck kinematics using a single
393 angle may partly explain this issue, as the cervical vertebral series is far from rigid, and displays
394 varying degrees of curvature over the course of a single stride (Video S1). A spline-based
395 analysis may yield a more robust parameter with which to investigate giraffes' neck kinematics.

396 The giraffes were studied in their natural habitat, meaning any conclusions can be more
397 confidently applied to giraffes as a wild species, compared with a laboratory setting where
398 conclusions are confined to a specific set of conditions. The drawback is that controlled
399 experimental conditions were not strictly possible. The effects of confounding variables were
400 kept to a minimum by only collecting data from relatively flat terrain, avoiding extremes of
401 weather conditions and comparing giraffes of similar size. Textured terrain models can be used
402 in future to quantify elevation, substrate type and other random effects. Such terrain parameters
403 may useful in investigating giraffes' athletic abilities and energetic costs.

404

405

406 **CONCLUSIONS**

407 This study was a novel application of a UAV system, and has highlighted the gains and technical
408 challenges of this method. We recommend that UAV users minimise kinematic measurement
409 error by maximising the focal distance and confining the study subject to the centre of the field
410 of view. Giraffes' lack of an intermediate gait was compensated for by their rotary galloping
411 gait; giraffes are slow gallopers. Duty factors were lower than predicted by dynamic similarity,
412 suggesting that galloping giraffes may experience high peak ground reaction forces. However, a
413 speed-dependent reduction in contralateral limb phase, and modest maximal speed may maintain
414 appropriate tissue safety factors.

415

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423

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Table 1 (on next page)

Details of study sites

1

	Size (hectares)	Number of giraffes	Giraffe temperament	Calibration methods used
Site 1	460	2	Tame	A,B,C
Site 2	250	6	Wild	C
Site 3	12500	27	Wild	C

2

Table 2 (on next page)

Comparison of MTP-C distance estimates from one giraffe in field site 1.

Method A resulted in the lowest standard deviation, and was used as the standard to which the other methods were compared. Method C was compared twice; once using artificial ground markers, once using naturally occurring features.

MTP-C distance estimate				
Method	Range (m)	Mean (m)	Standard deviation (m)	% error
A	0.78 - 0.84	0.814	0.018	
B	0.76 - 0.82	0.783	0.022	3.7
C _{natural}	0.74 - 0.88	0.850	0.099	4.9
C _{artificial}	0.76 - 0.83	0.784	0.024	3.7

1

Table 3 (on next page)

Comparison of power equations from the current dataset, with equations for dynamic similarity.

Data from Alexander and Jayes (1983) were digitised, with the exception of hind duty factor (*) which was not presented as a figure. Equations are in the form $y = a(Fr)^b$. The $\pm 95\%$ confidence interval is given in brackets where available. Relative stride length (stride length / leg length) in giraffes was consistent with the predictions for dynamic similarity; i.e. giraffes take proportionally similar strides. Fore and hind duty factors in giraffes were lower than predicted by dynamic similarity, as indicated by the significantly lower coefficient (a).

Stride parameter	Giraffe coefficients		Coefficients from Alexander and Jayes 1983	
	a	b	a	b
Relative stride length	1.98 (0.11)	0.31 (0.11)	1.85 (0.09)	0.43 (0.02)
Fore duty factor	0.44 (0.01)	-0.17 (0.06)	0.52 (0.02)	-0.27 (0.04)
Hind duty factor	0.41 (0.01)	-0.19 (0.07)	0.53*	-0.28 (0.03)*

1

Figure 1

A comparison of features from UAV footage, a 3D textured mesh and a photograph.

(A) Still frame of a galloping giraffe from UAV video. (B) Render from a textured 3D mesh, created from aerial photographs. The natural feature from the still image can be referenced to the textured 3D mesh. The feature was measured in the same plane as the hindlimb, and this measurement used to convert the MTP-C pixel distance (C) into an estimation of the metric distance.

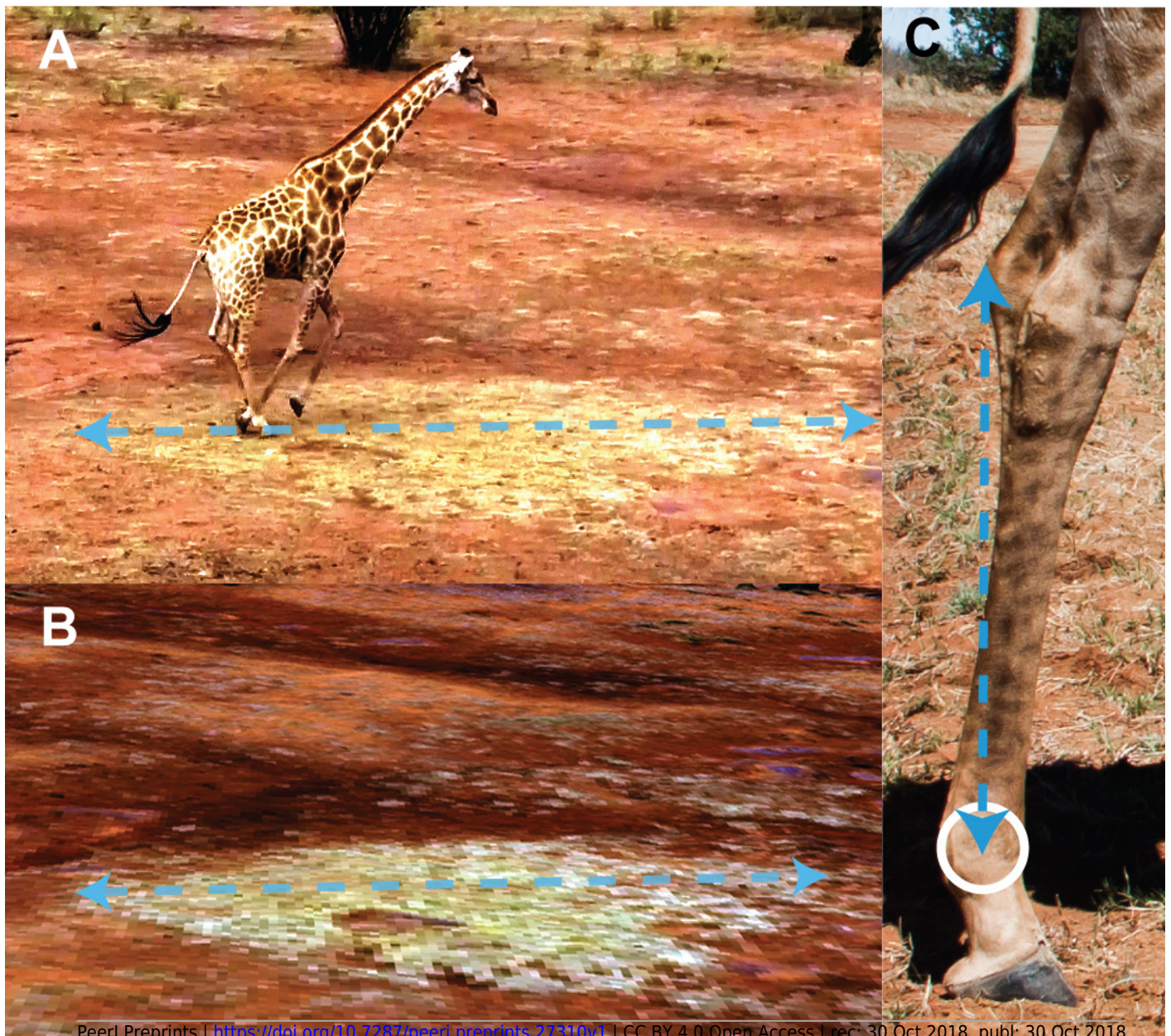


Figure 2

Neck and pitch angle time series during steady state rotary galloping

(A) The anatomical definitions of neck angle and body pitch, demonstrated in a standing individual. Neck angle (B) and body pitch (C) time series from strides commencing with foot-ground contact by the non-leading hindlimb, with mean time series (thicker line).

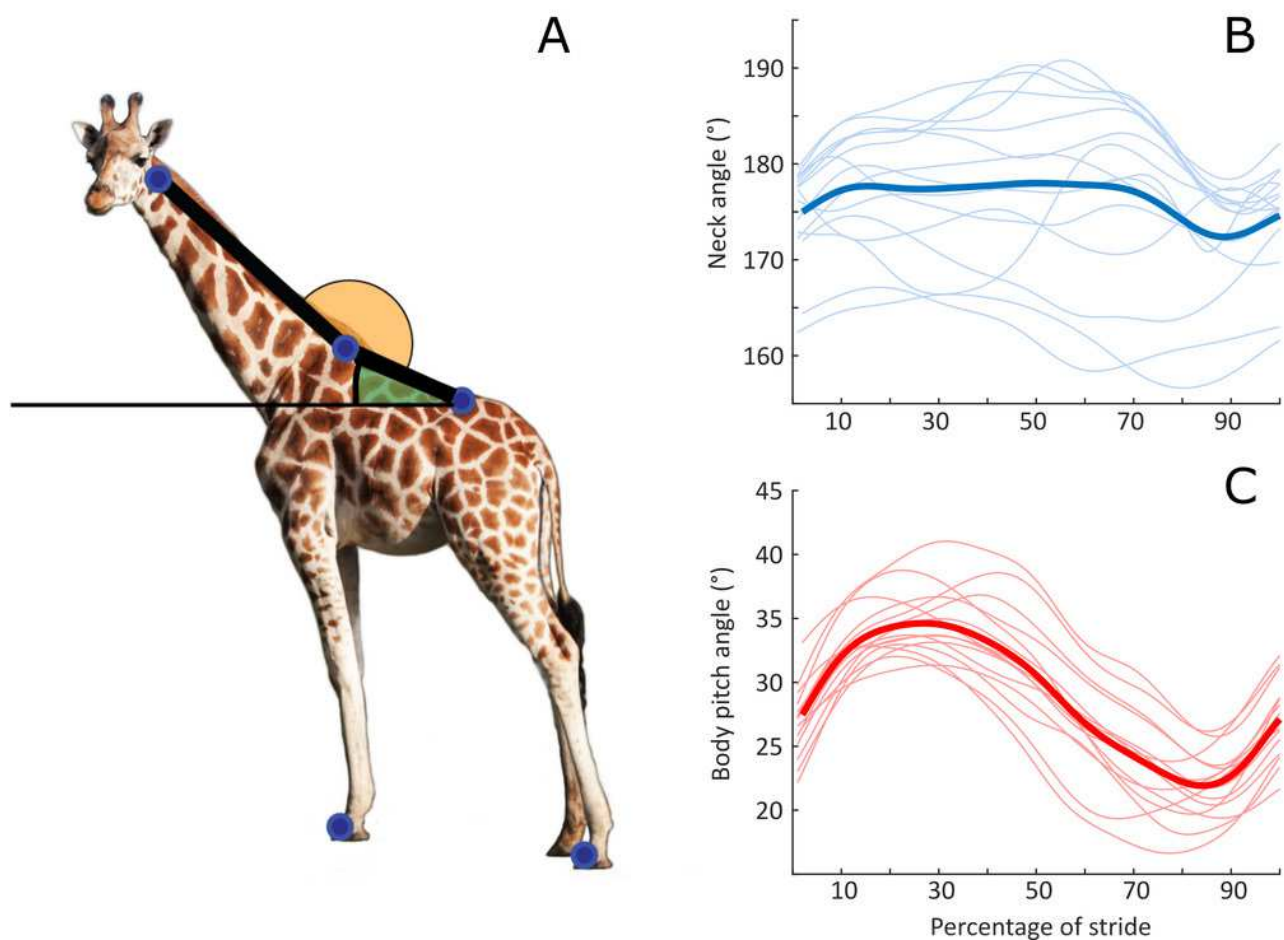


Figure 3(on next page)

Box and whisker plot showing percentage error of UAV derived speed measurements compared to treadmill speed, with overlying data points.

Human running speed measured by the UAV was most accurate when the subject was furthest distance, and when they were centred in the field of view.

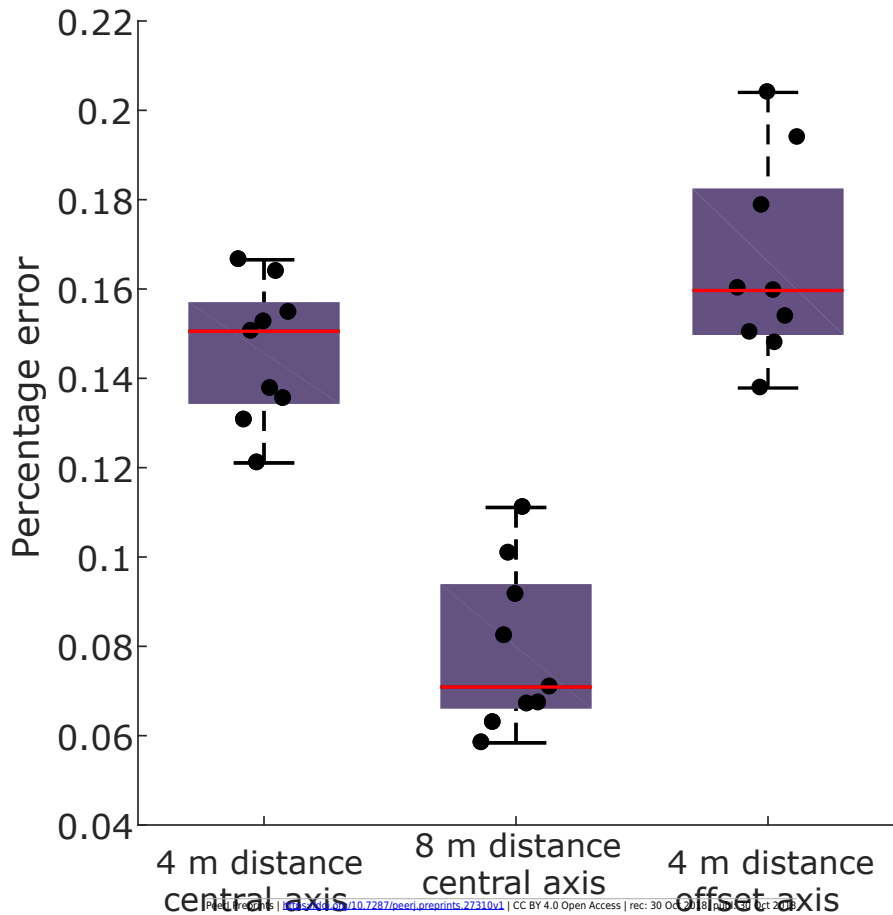
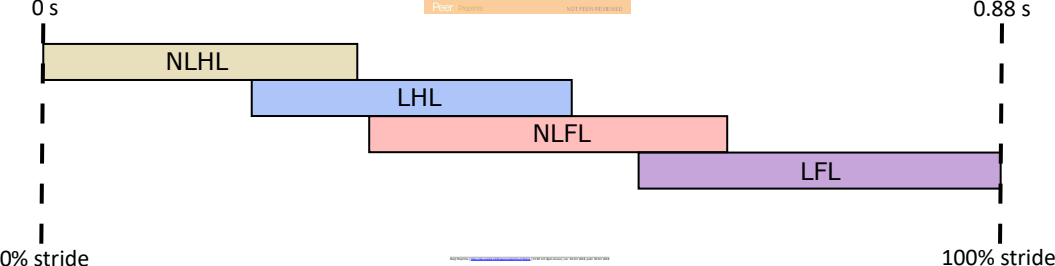


Figure 4(on next page)

Footfall sequence of a representative stride from a giraffe running at 4.88 ms^{-1} , with a forelimb duty factor of 0.39 and hindlimb duty factor of 0.38.



0% stride

100% stride

Figure 5(on next page)

Change in stride length (m) and stride frequency (Hz) as a function of speed (ms^{-1})

Stride length (A) changed by 0.55 m per unit of speed (u): $y = 0.55u + 1.43$, $R^2 = 0.63$, $p < 0.001$. Stride frequency (B) changed by 0.05 Hz for every unit of speed (u): $y = 0.05u + 0.88$, $R^2 = 0.66$, $p < 0.001$.

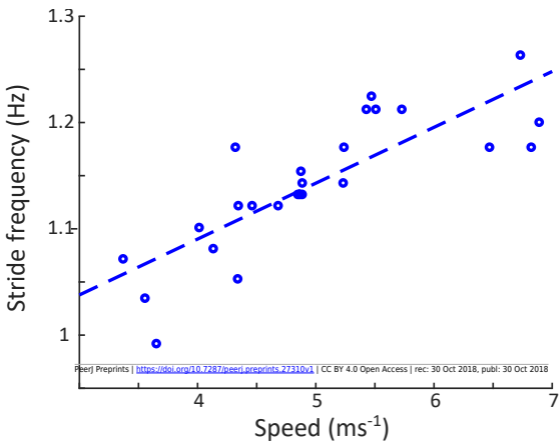
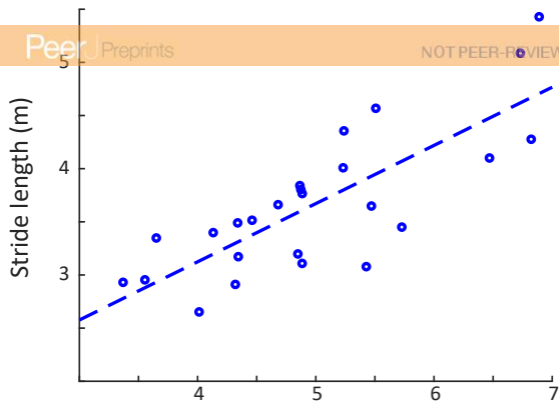


Figure 6(on next page)

Changes in stance duration (s), swing duration (s) and duty factor as a function of speed (ms^{-1})

(A) Stance duration was longer in the forelimb (blue circles) than the hindlimb (red circles), and both decreased with speed (FL: $y = -0.04u + 0.57$, $R^2 = 0.70$, $p < 0.001$; HL: $y = -0.04u + 0.55$, $R^2 = 0.74$, $p < 0.001$). Swing duration (B) was independent of speed, resulting in a duty factor (C) which was greater in the forelimb than the hindlimb, and which decreased with speed (FL: $y = -0.03u + 0.55$, $R^2 = 0.49$, $p < 0.001$; HL: $y = -0.03u + 0.53$, $R^2 = 0.54$, $P < 0.001$).

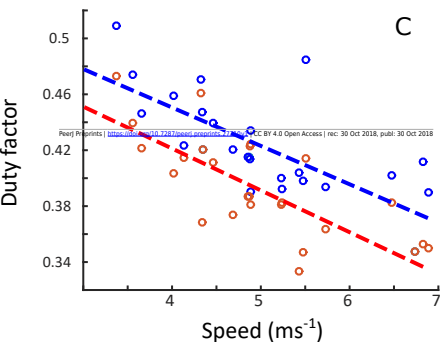
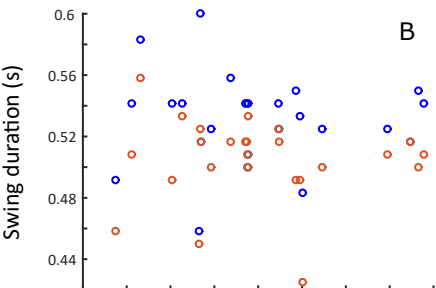
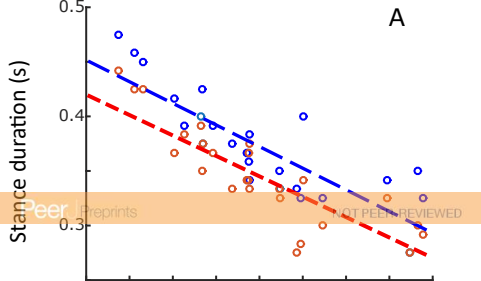


Figure 7 (on next page)

Changes in contralateral limb phase as a function of speed (ms^{-1})

Contralateral limb phase is expressed as the relative lag time between footfalls of the left and right side. Phase was greater in the forelimb than the hindlimb, and decreased with speed. A decrease in phase indicated that the overlap between left and right footfalls was greater at faster speeds (FL: $-0.01u + 0.36$, $R^2 = 0.35$, $p = 0.002$; HL: $y = -0.02u + 0.29$, $R^2 = 0.57$, $p < 0.001$).

Phase

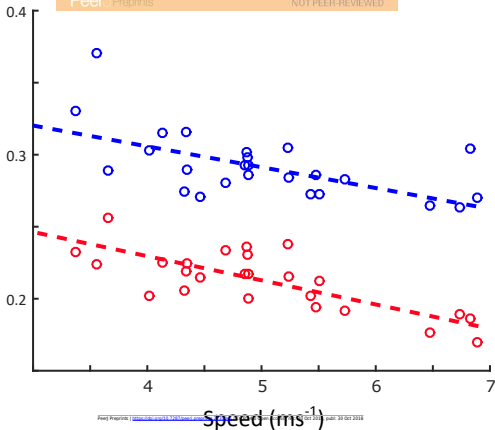


Figure 8

A still image of a rotary galloping giraffe taken from video footage recorded using a DJI Phantom 4 UAV, at study site 3.

We recommend that kinematic analyses of the study subject is confined to the centre box of a 3x3 grid, overlying the field of view. Linear and angular measurements outside of this area will be subject to greater parallax error.

